Report No. 11b (Spl).

Lloyd's Register of Shipping.

SURVEYS FOR FREEBOARD—STEAMERS.

Index No. 32215
(For London Office only.)
Port of Survey Dundee
Date ~~of Survey~~ 12/1/31
Name of Surveyor —

Ship's Name.	Port of Registry and Nationality.	Official Number.	Gross Tonnage.	Date of Build.	Particulars of Classification.
BRITISH FAITH.	British	149974	—	1927.	+100A1 Carrying Petroleum in Bulk.

Number in Register Book

Moulded dimensions 440·0 × 56·75 × 33·92
Moulded displacement at a moulded draught of 85 per cent. of moulded depth See Back.
Coefficient of fineness for use with tables ·781

DEPTH FOR FREEBOARD.

Moulded depth	33·92
Stringer plate	·06
Sheathing in wells $T\left(\frac{L-S}{L}\right)$ =	—
Depth D =	33·98

CORRECTION FOR LENGTH.

(a) When D is greater than $\frac{L}{15}$
$\left(D-\frac{L}{15}\right) \times R = (33·98 - 29·33) \times 3$ = +13·95

(b) When D is less than $\frac{L}{15}$ (if allowed).
$\left(\frac{L}{15}-D\right) \times R$ = —

If restricted by height of superstructures —

SUPERSTRUCTURES.

	Mean Covered Length S.	Equivalent Enclosed Length S_1.	Height.	Correction for Height.	Effective Length.
Poop enclosed	103·14	103·14	8'-0"	—	103·14
„ overhang					
R.Q.D. enclosed					
„ overhang					33·83
Bridge enclosed	33·83	33·83	8'-0"	—	
„ overhang aft					
„ overhang forward					
F'cle enclosed	53·58	49·64	8'-0"	—	49·64
„ overhang					
Trunks forward					
„ aft					
Tonnage opening					
TOTAL =	190·58	186·64			186·64
Length of ship (L) =	440·0	440·0			440·0
% Covered =	43·31	42·42			42·42

SHEER AFT.

Actual			Standard		
51·5	1	51·5	54·0	1	54·0
12·0	3	36·0	24·0	3	72·0
−1·5	3	−4·5	6·0	3	18·0
—	1	—	—	1	—
		83·0			144·0

Sheer aft = $\frac{83·0}{144·0}$ 57·64% of Standard

Corresponding %, corrected for absence of forecastle if required { A = Lanker B = 33·42
Allowance = 42·00 × ·3342 = −14·04
Correction for Bridge less than ·2L if required { Lanker

SHEER.

Station.		Actual Sheer.	Standard Sheer.	Allowed Sheer.	S. M.	Products.
A.P.	1	51·5	54·0	51·5	1	51·5
	2	12·0		12·0	4	48·0
	3	−1·5		−1·5	2	−3·0
	4	—	—	—	4	—
	5	18·5	12·0	13·99	2	24·98
	6	52·45	48·0	49·45	4	197·80
F.P.	7	105·5	108·0	105·5	1	105·5
					18	427·78

Mean effective sheer = 23·77
Standard sheer ·05L + 5 = 24·00
Difference (Df) = 3·23
Allowance = $Df \times \left(·75 - \frac{S}{2L}\right)$ = 3·23 × (·75 − ·2165) = +1·72
If limited on account of amidship superstructure =
If limited on account of excess sheer ($1\frac{1}{2}$ in. per 100 ft.) =

If excess sheer forward and deficient sheer aft :—

$\frac{\text{Actual sheer aft}}{\text{Standard sheer aft}}$ = Deficient 57·64% of Standard

$\frac{\text{Actual sheer forward}}{\text{Standard sheer forward}}$ = Excess.

$\frac{\text{Length of enclosed superstructure}}{L}$

Forward of amidships = { Lanker
Aft of amidships =

ROUND OF BEAM.

Standard	13·62
Ship	14·00
Difference	·38
Restricted to	
Allowance = $\frac{\text{Difference}}{4} \times \left(1-\frac{S_1}{L}\right)$ =	·38/4 × ·5458 = −·05

TABULAR FREEBOARD (corrected for flush deck if required) = 42·50.

Corrected for Coefficient ·781 $\frac{+·68}{1·36}$ = 1·044 = 44·89

	+	−
Correction for Length	13·95	
„ Superstructures		14·04
„ Sheer	1·72	
„ Round of beam		·05
„ Thickness of deck	—	
„ Scantlings, etc.	—	
„ Statutory deck line	—	
	15·67	14·09
	+ 1·58	

Summer Freeboard = 44·47

33·98 + 6·62 = 40·60 ÷ 4 = 10·15 + 6·84 = 16·99
49·47 + 6·84 = 56·31

FREEBOARD recommended amidships from centre of Disc to top of Statutory Deck Line, ~~Wood~~ (Steel) Deck :— 6'-4½"

Fresh Water Line	above centre of Disc	
Indian Summer Line	„ „ „	4'-2¼"
Winter Line	below „ „	
Winter North Atlantic Line	„ „ „	

1906 Tabdo. 4'-4¾" 8'-2" } Diffo S = −12¼ W = −11¾

5c.7.30.

© 2020 Lloyd's Register Foundation
002024-002037-0030

actual	0	18·5	52·47½°	105·45
Standard	0	12·0	48·0	108·0
diff	0	6·5	4·47½°	-
× 7·64/26	0	1·99	1·45°	-
Standard	0	12·0	48·0	-
allowed	0	13·99	49·45°	105·5°

85% of 33·92 = 28·832

= 28-10

26-4½

2-5½

Ext Δ d. @ 26-4½" mld. = 14680

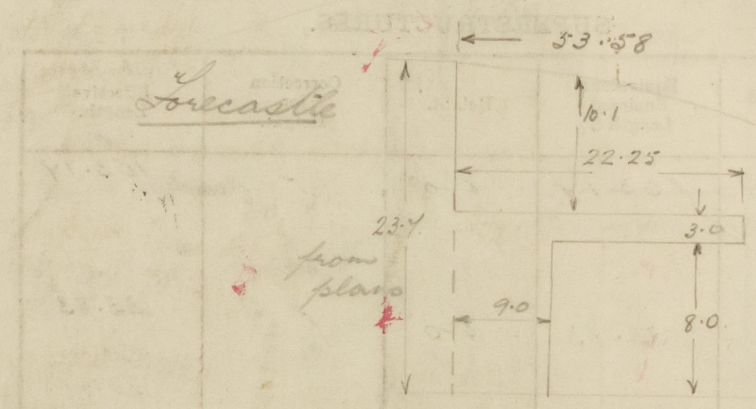
29½ @ 49·5° = 1460

16140

$$B.C. = \frac{16140 \times .995 \times 35}{440 \times 56·75 \times 28·832}$$

$$= .781$$

Forecastle



53·58
22·25
31·33

22·25
9·00
13·25

Closed 31·33

Sidehouses $\frac{22·25 \times 10·1}{23·4} = 9·91$

Centrehouse $\frac{13·25 \times 8}{23·4} = 4·54$

45·71

53·58
45·71
2 | 7·87
3·93
45·71
49·64

© 2020
Lloyd's Register Foundation